

IN THE CLAIMS

Please amend the claims as follows:

Claim 1 (Currently Amended): A process for the conversion of heavy feedstocks selected from the group consisting of heavy crude oils, distillation residues, heavy oils coming from catalytic treatment, thermal tars, bitumens from oil sands, ~~various kinds of coals~~ and ~~other high-boiling feedstocks of a hydrocarbon origin known as black oils~~, by the combined use of the following three process units: hydroconversion with catalysts in slurry phase (HT), distillation or flash (D), and deasphalting (SDA), ~~comprising the following steps:~~

mixing at least part of the heavy feedstock and/or at least most of ~~the~~ a stream containing asphaltenes obtained in ~~the~~ a deasphalting unit with a ~~suitable~~ hydrogenation catalyst and sending the mixture obtained to a hydrotreatment reactor (HT) into which hydrogen or a mixture of hydrogen and H<sub>2</sub>S is charged;

sending ~~the~~ a stream containing the hydrotreatment reaction product and the catalyst in dispersed phase to one or more distillation or flash steps (D) whereby ~~the~~ different fractions coming from the hydrotreatment reaction are separated; and

recycling at least part of ~~the~~ a distillation residue (tar) or liquid leaving ~~the~~ a flash unit, comprising the catalyst in dispersed phase, rich in metal sulfides produced by demetallation of the feedstock and possibly coke, to ~~the~~ a deasphalting zone (SDA) in the presence of solvents, optionally also fed with at least a fraction of the heavy feedstock, obtaining two streams, one consisting of deasphalted oil (DAO) and the other containing asphaltenes,

wherein a fraction of the stream containing asphaltenes, coming from the deasphalting section (SDA), called flushing stream, is sent to a treatment section with ~~a-suitable~~ added solvent for the separation of the product into a solid fraction and a liquid fraction from which said solvent can be subsequently removed.

Claim 2 (Original): The process according to claim 1, wherein the flushing stream is in a quantity ranging from 0.5 to 10% by volume with respect to the fresh feedstock.

Claim 3 (Currently Amended): The process according to claim 1, wherein at least part of the liquid fraction deriving from the treatment section ~~of the flushing~~ is sent as such or after being separated from the solvent and/or after the addition of a suitable fluxing liquid to the Fuel Oil fraction.

Claim 4 (Currently Amended): The process according to claim 1, wherein at least part of the liquid fraction deriving from the treatment section ~~of the flushing~~ is recycled to the hydrotreatment reactor (HT).

Claim 5 (Currently Amended): The process according to claim 1, wherein the solvent used in the treatment section ~~of the flushing~~ is an aromatic solvent or a mixture of gas oils produced in the process itself or available in refineries.

Claim 6 (Currently Amended): The process according to claim 5, wherein the solvent is an aromatic solvent is selected from the group consisting of toluene and/or a mixture of xylenes.

Claim 7 (Original): The process according to claim 1, wherein the volumetric ratio solvent/flushing stream varies from 1 to 10.

Claim 8 (Original): The process according to claim 7, wherein the volumetric ratio solvent/flushing stream varies from 1 to 5.

Claim 9 (Original): The process according to claim 8, wherein the volumetric ratio solvent/flushing stream varies from 1.5 to 3.5.

Claim 10 (Previously Presented): The process according to claim 1, wherein all the heavy feedstock is mixed with a suitable hydrogenation catalyst and sent to the hydrotreatment reactor (HT), whereas at least 60% of the stream containing asphaltenes, which also comprises catalyst in dispersed phase and possibly coke and is enriched with metals coming from the initial feedstock, is recycled to the hydrotreatment zone.

Claim 11 (Original): The process according to claim 10, wherein at least 80% of the stream containing asphaltenes is recycled to the hydrotreatment zone.

Claim 12 (Previously Presented): The process according to claim 1, wherein part of the heavy feedstock and at least most of the stream containing asphaltenes, which also contains catalyst in dispersed phase and possibly coke, are mixed with a suitable hydrogenation catalyst and sent to the hydrotreatment reactor, whereas the remaining part of the heavy feedstock is sent to the deasphalting section.

Claim 13 (Previously Presented): The process according to claim 1, wherein at least most of the stream containing asphaltenes, which essentially consists of said asphaltenes, is mixed with a suitable hydrogenation catalyst and sent to the hydrotreatment reactor, whereas all the heavy feedstock is fed to the deasphalting section.

Claim 14 (Original): The process according to claim 1, wherein part of the distillation residue (tar) or liquid leaving the flash unit is recycled to the deasphalting zone (SDA) and at least part of the remaining part of said distillation or flash residue is sent to the hydrotreatment reactor.

Claim 15 (Original): The process according to claim 14, wherein at least part of the distillation or flash residue is sent to the hydrotreatment reactor together with at least part of the stream containing asphaltenes coming from the deasphalting section (SDA).

Claim 16 (Original): The process according to claim 1, wherein at least 80% by weight of the distillation residue is recycled to the deasphalting zone.

Claim 17 (Original): The process according to claim 16, wherein at least 95% by weight of the distillation residue is recycled to the deasphalting zone.

Claim 18 (Original): The process according to claim 1, wherein at least part of the remaining quantity of distillation residue (tar), not recycled to the deasphalting zone is recycled to the hydrotreatment section.

Claim 19 (Original): The process according to claim 1, wherein the distillation steps are carried out at a reduced pressure ranging from 0.0001 to 0.5 MPa.

Claim 20 (Original): The process according to claim 19, wherein the distillation steps are carried out at a reduced pressure ranging from 0.001 to 0.3 MPa.

Claim 21 (Original): The process according to claim 1, wherein the hydrotreatment step is carried out at a temperature ranging from 370 to 480°C and at a pressure ranging from 3 to 30 MPa.

Claim 22 (Original): The process according to claim 21, wherein the hydrotreatment step is carried out at a temperature ranging from 380 to 440°C and at a pressure ranging from 10 to 20 MPa.

Claim 23 (Original): The process according to claim 1, wherein the deasphalting step is carried out at temperature ranging from 40 to 200°C and at a pressure ranging from 0.1 to 7 MPa.

Claim 24 (Original): The process according to claim 1, wherein the deasphalting solvent is a light paraffin with from 3 to 7 carbon atoms.

Claim 25 (Original): The process according to claim 1, wherein the deasphalting step is carried out under subcritical or supercritical conditions with one or more steps.

Claim 26 (Original): The process according to claim 1, wherein the stream consisting of deasphalted oil (DAO) is fractionated by means of conventional distillation.

Claim 27 (Original): The process according to claim 1, wherein the stream consisting of deasphalted oil (DAO) is mixed with the products separated in the distillation step after being condensed.

Claim 28 (Original): The process according to claim 1, wherein the hydrogenation catalyst is a decomposable precursor or a preformed compound based on one or more transition metals.

Claim 29 (Original): The process according to claim 28, wherein the transition metal is molybdenum.

Claim 30 (Original): The process according to claim 1, wherein the concentration of the catalyst in the hydroconversion reactor, defined on the basis of the concentration of the metal or metals present, ranges from 300 to 20000 ppm.

Claim 31 (Original): The process according to claim 30, wherein the concentration of the catalyst in the hydroconversion reactor ranges from 1000 to 10000 ppm.

Claim 32 (Previously Presented): The process according to claim 1, wherein the stream containing the hydrotreatment reaction product and the catalyst in dispersed phase, before being sent to one or more distillation or flash steps, is subjected to a high pressure separation pre-step in order to obtain a light fraction and a heavy fraction, the heavy fraction alone being sent to said distillation step(s) (D).

Claim 33 (Previously Presented): The process according to claim 32, wherein the light fraction obtained by the high pressure separation step is sent to a secondary post-treatment hydrogenation section, producing a lighter fraction containing C<sub>1</sub>-C<sub>4</sub> gas and H<sub>2</sub>S and a heavier fraction containing hydrotreated naphtha and gas oil.

Claim 34 (Original): The process according to claim 33, wherein the post-treatment hydrogenation reaction is effected at a pressure ranging from 7 to 14 MPa.

Claim 35 (Previously Presented): The process according to claim 1, wherein the solid fraction of the product treated is sent to a further selective recovery treatment of the transition metal(s) contained in the hydrogenation catalyst.

Claim 36 (Original): The process according to claim 35, wherein the transition metal(s) recovered, is recycled to the hydrotreatment reactor (HT).

Claim 37 (New): The process according to claim 1, wherein the fraction of the stream containing asphaltenes, coming from the deasphalting section (SDA), is sent to the treatment section with added solvent and separated into a solid fraction and a liquid fraction from which said solvent is subsequently removed under subcritical conditions.

Claim 38 (New): The process according to claim 1, wherein the fraction of the stream containing asphaltenes, coming from the deasphalting section (SDA), is sent to the treatment section with added solvent and separated into a solid fraction and a liquid fraction from which said solvent is subsequently removed under supercritical conditions.